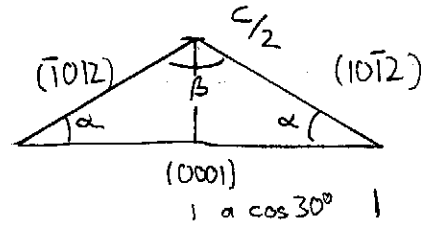


# Problem #1:

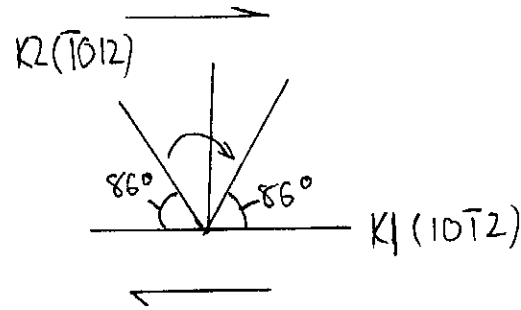


$$\tan \alpha = \frac{c/2}{a \cos 30^\circ} \stackrel{c/a = 1.86}{=} \frac{1.86a/2}{a \cos 30^\circ} = 1.07$$

$$\Rightarrow \alpha = 47^\circ$$

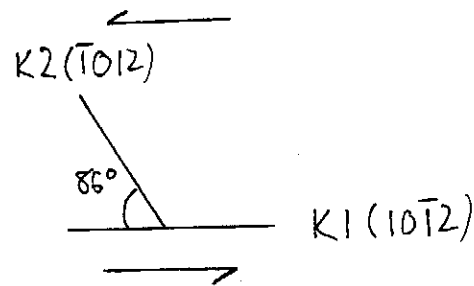
$$\Rightarrow \beta = 180^\circ - 2\alpha = 86^\circ$$

tension



twins ✓

compression



twinning not possible

- calc.  $\beta$  ✓
- tension and compression ✓
- $c/a$  ratio ✓

## Problem #2:

closed packed  $c/a = 1.633$

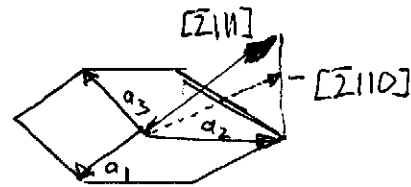
$\Rightarrow \beta > 90^\circ \Rightarrow$  twins in compression e.g. Mg ( ~~$c/a = 1.624$~~ )

- $c/a$  ration for closed packed ✓
- $\beta > 90^\circ$  ✓
- twins in compression ✓

Problem #3:

Tension  $[\bar{2}11]$

slip system in hcp  $\{000\} \langle 11\bar{2}0 \rangle \rightsquigarrow$



- $[11\bar{2}0]$
- $[\bar{2}110]$
- $[1\bar{2}10]$
- $[\bar{1}\bar{1}20]$
- $[\bar{2}\bar{1}\bar{1}0]$
- $[\bar{1}2\bar{1}0]$

$\rightsquigarrow$  maximum stress  $\rightsquigarrow [\bar{2}110]$

Problem #4:

$$(111)[11\bar{2}]$$

$$K_1 = (111) \quad K_2 = (11\bar{1})$$

$$\text{normal vectors } \vec{K}_1 = [111] \quad \vec{K}_2 = [11\bar{1}]$$

$$\vec{K}_1 \cdot \vec{K}_2 = |\vec{K}_1| |\vec{K}_2| \cos \alpha$$

$$\Rightarrow \alpha = \cos^{-1}\left(\frac{1}{3}\right) \approx 70.5$$

$$\beta = 180^\circ - 2\alpha = 38.9 \approx 39^\circ$$

$$\gamma = 2 \tan(90^\circ - \alpha) = 0.708$$

or through geometrical considerations

- calc ✓ (angle + strain)
- geometrical considerations ✓

## Problem #5:

tension rotates towards 101

furthest away is ~~110~~ 110

$$\cos \alpha = \frac{\begin{pmatrix} 1 \\ 0 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 0 \end{pmatrix}}{\sqrt{2} \cdot \sqrt{2}} = \frac{1}{2} \Rightarrow \alpha = 60^\circ \Rightarrow \theta = 30^\circ \text{ before other slip system is activated}$$

- find right directions ✓

- angle calc ✓

Problem #6:

use dislocation densities in shear equation

$$\Rightarrow D_1 t_1 = D_2 t_2 \quad t_2 = t_1/2 \quad \Rightarrow 2D_1 = D_2$$

$$\Rightarrow \frac{D_2}{D_1} = 2$$

$$D_i = D_0 \exp[-Q/RT]$$

$$\Rightarrow \frac{\exp[-Q/RT_2]}{\exp[-Q/RT_1]} = 2 \Rightarrow \exp\left[-Q\left(\frac{1}{RT_1} - \frac{1}{RT_2}\right)\right] = 2$$

$$\ln 2 = Q\left(\frac{1}{RT_2} - \frac{1}{RT_1}\right) \Rightarrow Q = \frac{RT_1 T_2}{T_1 - T_2} \cdot \ln 2 = 630 \frac{\text{kJ}}{\text{mol}}$$

$$\left[ \frac{\text{J}}{\text{mol} \cdot \text{K}} \cdot \text{K} \cdot \text{K} = \frac{\text{J}}{\text{mol}} \right] \checkmark$$

depending on reference:  $Q \hat{=} W, Nb$

- calc.  $\checkmark$   
-  $Q \checkmark$

Problem #7:

Yes,  $T_m = 3695\text{K} \Rightarrow T > \frac{1}{3} T_m$  + short explanation (see lecture)

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3.40J / 22.71J / 3.14 Physical Metallurgy  
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