

Foams: Microstructural Design

- foams - behaviour dominated by cell wall bending
- foam properties can be increased by increasing EI of cell walls

Hollow walls



thin walled tube $I_t = \pi r^3 t$

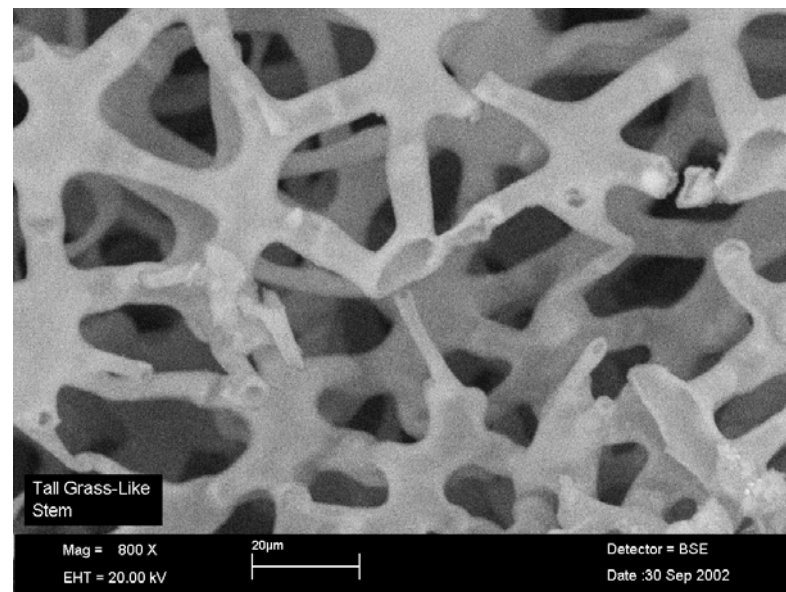
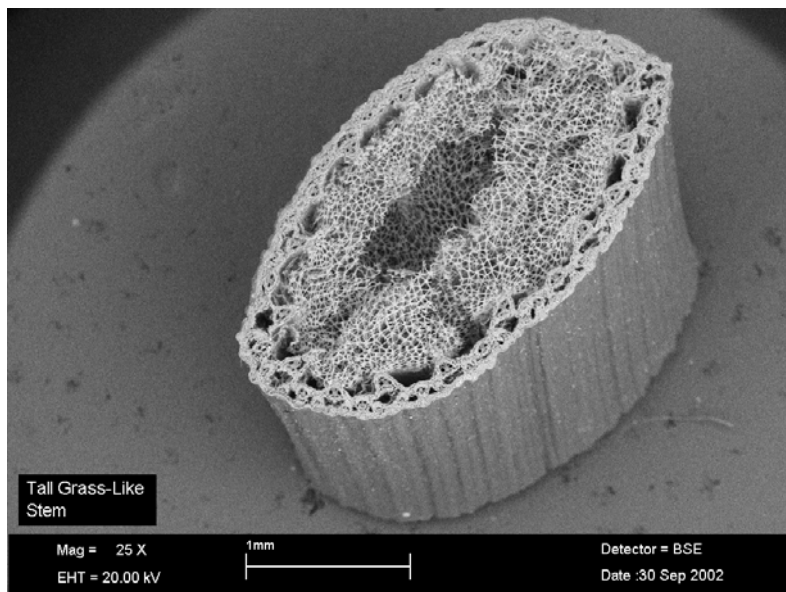
solid circular section $I_s = \frac{\pi R^4}{4}$

masses equal: $\pi R^2 = 2\pi r t$
 $R = \sqrt{2rt}$

$$\frac{I_t}{I_s} = \frac{4\pi r^3 t}{\pi R^4} = \frac{4r^3 t}{4r^2 t^2} = \frac{r}{t}$$

$$\therefore \frac{E^*_{\text{tube wall}}}{E^*_{\text{solid wall}}} \propto \frac{r}{t}$$

- can do similar analysis for other properties



Sandwich cell walls

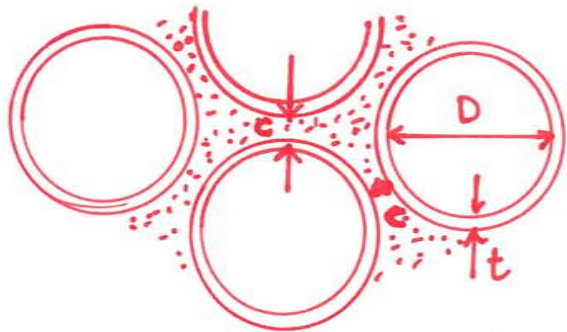
- sandwich beam - two stiff faces separated by a lightweight core
 - core typically a honeycomb or foam (or balsa)



I-beam effect - increase in moment of inertia, with little increase in weight

faces - like flanges of I beam - resist bending
 core - " web " " " - " shear

- microsandwich foam



$d = \text{foam cell size}$

microsandwich foam

- thin walled hollow spheres distributed in a foam
- have to get geometry right
- require:

Spheres: $t \ll D$
 $E_{\text{sphere}} \gg E_{\text{foam}}$
 $V_{\text{spheres}} \approx 50-60\%$

foam: $d \ll c$

Foams: Microstructural design

- another alternative is to use microstructure that induces axial, rather than bending, deformations
- 3D lattice materials - triangulated trusses in 3D
 - forces in members all axial; bending negligible
- various processing methods + geometries possible - all triangulated
- can analyze truss as having pin joints - axial forces in members
- open-cell structures

$$E^* = \frac{\sigma}{\epsilon} \propto \frac{F}{l^2} \frac{l}{\delta} \quad \delta \propto \frac{Fl}{AE_s} \propto \frac{Fl}{t^2 E_s}$$

$$E^* \propto \frac{F}{l} \frac{E_s t^2}{Fl} \propto E_s \left(\frac{t}{l}\right)^2 \propto E_s \left(\frac{\rho^*}{\rho_s}\right)$$

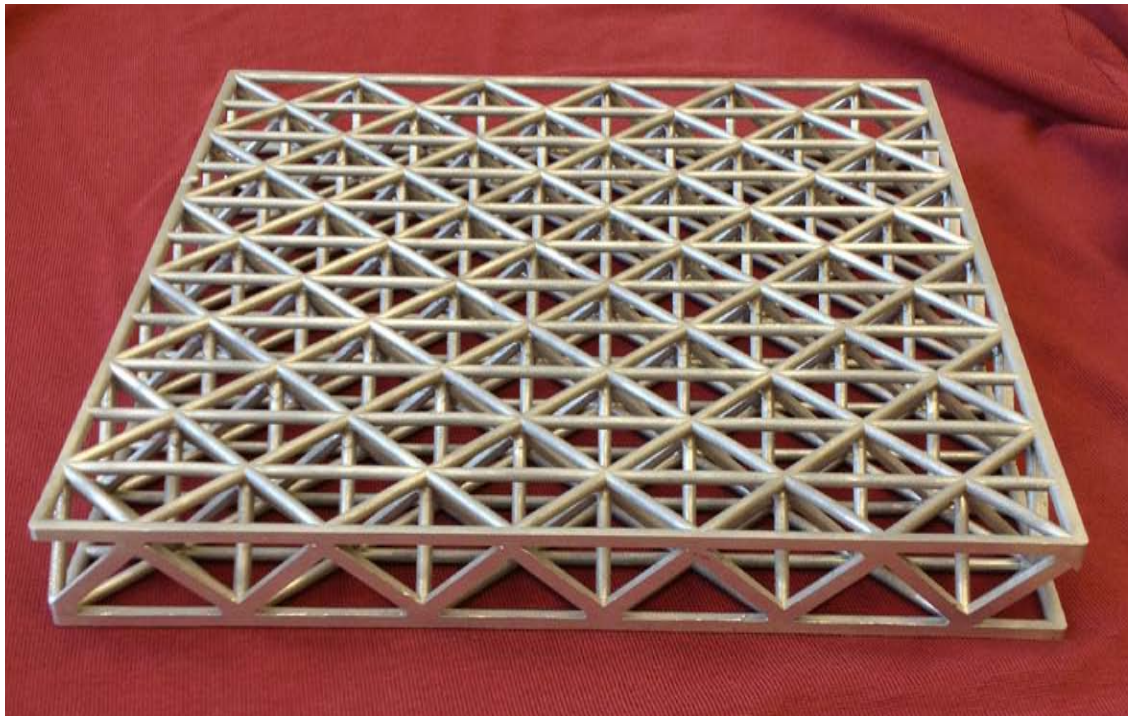
$$\boxed{E^* = C E_s (\rho^*/\rho_s)}$$

C depends on cell geometry + loading direction

• strength: if struts fail by uniaxial yield

$$\sigma_{pl}^* = C \sigma_{ys} (\rho^*/\rho_s)$$

But some struts in compression - may buckle (generally do buckle)



Compressive strut buckling

- elastic buckling $\sigma_{el}^* = C E_s (\rho^*/\rho_s)^2$ (like an open-cell foam)
 - if interaction between elastic buckling + yield - use a reduced modulus (tangent modulus)
 - also: imperfections such as non-straight struts or misaligned struts reduce buckling resistance
"knock-down" factor can be significant ~ 50%.
-

Material selection

- how to select the best material for some mechanical requirement?
- section on wood: derived performance index for minimizing mass of a beam of a given stiffness: $E^{1/2}/\rho$
- here, discuss materials selection more broadly
- another example: What material minimizes the mass of a beam of a given failure load, P_f ?
given P_f , span l , square cross-section t^2

$$\sigma_{\max} = \frac{My}{I}$$

$$\sigma_{\max} \propto \frac{P_f l t}{t^4} \propto \sigma_f$$

$$t \propto \left(\frac{P_f l}{\sigma_f} \right)^{1/3}$$

$$\text{mass, } m = \rho t^2 l$$

$$m \propto \rho \left(\frac{P_f l}{\sigma_f} \right)^{2/3} l$$

M = Maximum moment in beam $\propto P l$
 y = maximum distance from neutral axis $\propto t$
 I = moment of inertia $\propto t^4$
 σ_f = failure stress of beam material

Performance index: $\sigma_f^{2/3} / \rho$
 to be maximized

Materials selection

Ashby
book -
Tables

- can obtain performance indices for various loading configurations + mechanical requirements
- if plot data for material properties on log-log scales, performance indices appear as straight lines
- shifting lines up + down identifies best material for that performance index

CMM
Fig 7.1

· example: modulus - density chart

E/ρ : axially loaded tie of given stiffness

$E^{1/2}/\rho$: beam of given stiffness

$E^{1/3}/\rho$: plate " " "

Property charts for foams

CS Fig 13.1 E^* vs ρ^* : range of E^* factor of 10^6 , from 0.01 MPa to 10 GPa

Fig 13.2 σ^* vs ρ^* : range of σ^* from 10^{-3} to 30 MPa

⇒ scope for matching foam properties to design requirements

E^*/ρ vs σ^*/ρ : end grain balsa, metal foams high values

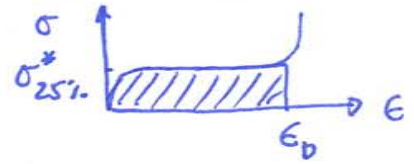
useful for sandwich panels - selection of core material

Property charts - foams

E_D vs. $\sigma_{25\%}^*$: contours show energy absorption/volume, U

$$U \sim \sigma_{25\%}^* E_D$$

$$E_D = U / \sigma_{25\%}^*$$



contours have slope of -1 on log-log scales

balca, metal foams - high values of U

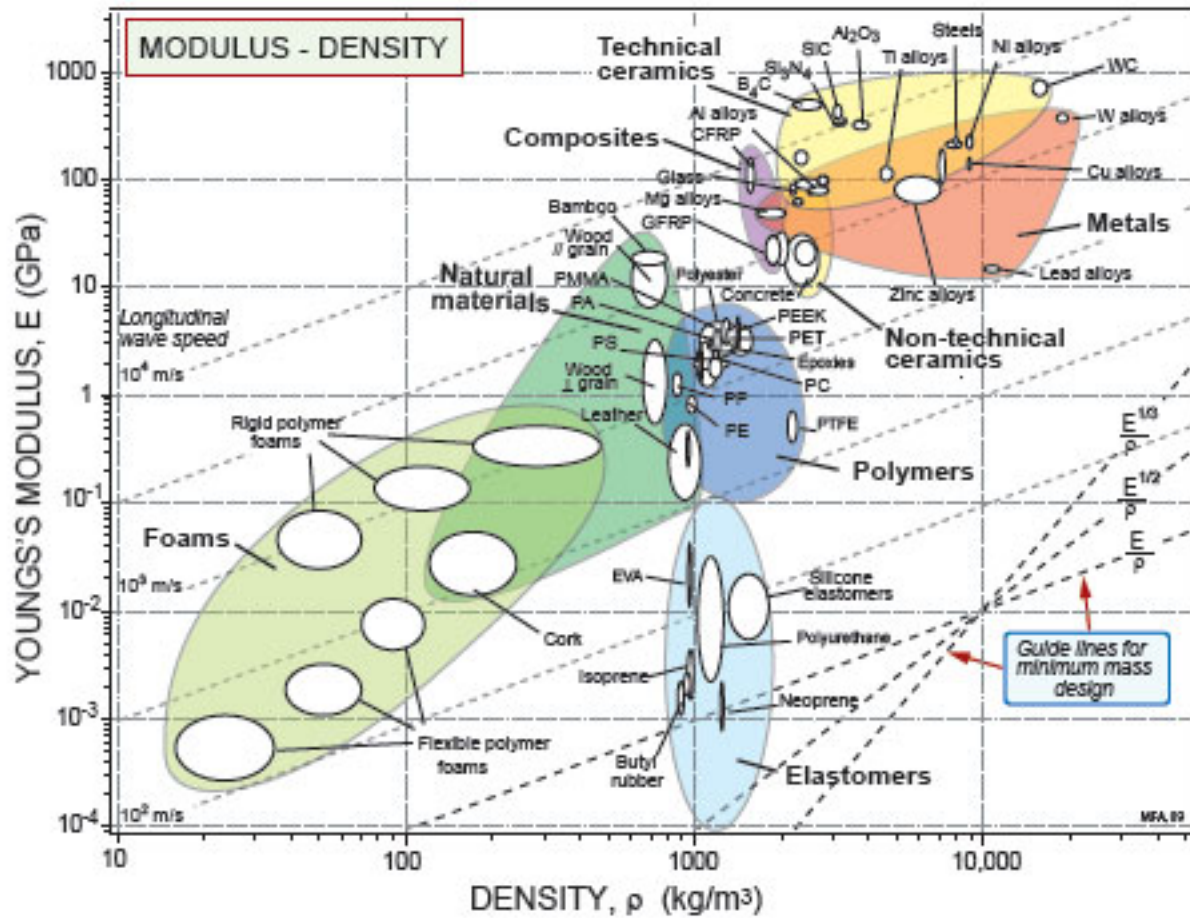
- can also produce selection charts for other properties - e.g. thermal
- λ vs $\sigma_{5\%}^*$
 - thermal conductivity, λ
 - thermal insulation applications usually have constraint on strength, too.
- λ vs T_{max} - may have constraint on maximum service temperature, too.
- density plot - closed cell foams - buoyancy
- cell size - open cell foams - filtration + catalysis
 - surface area/volume increases as cell size decreases
 - e.g. ceramic foams used in filtration of liquid metals

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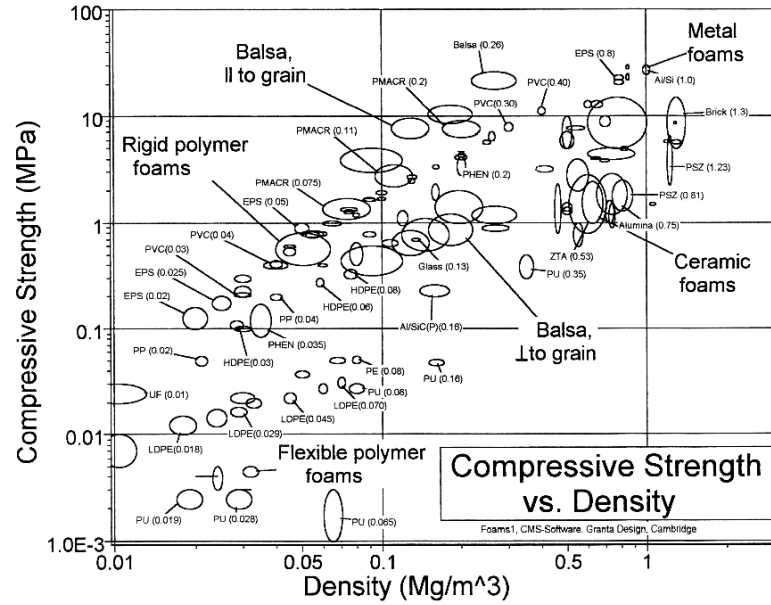
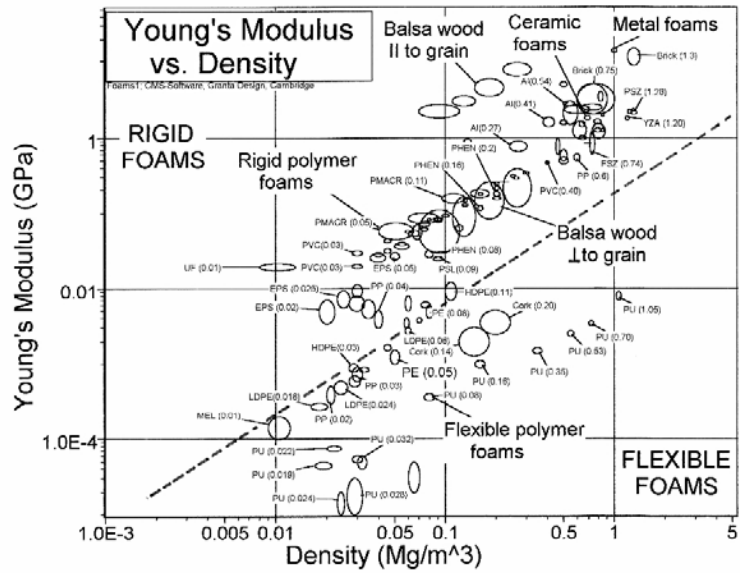
Ashby MF (1999) *Materials Selection in Mechanical Design*.
Second Edition Butterworth Heinemann

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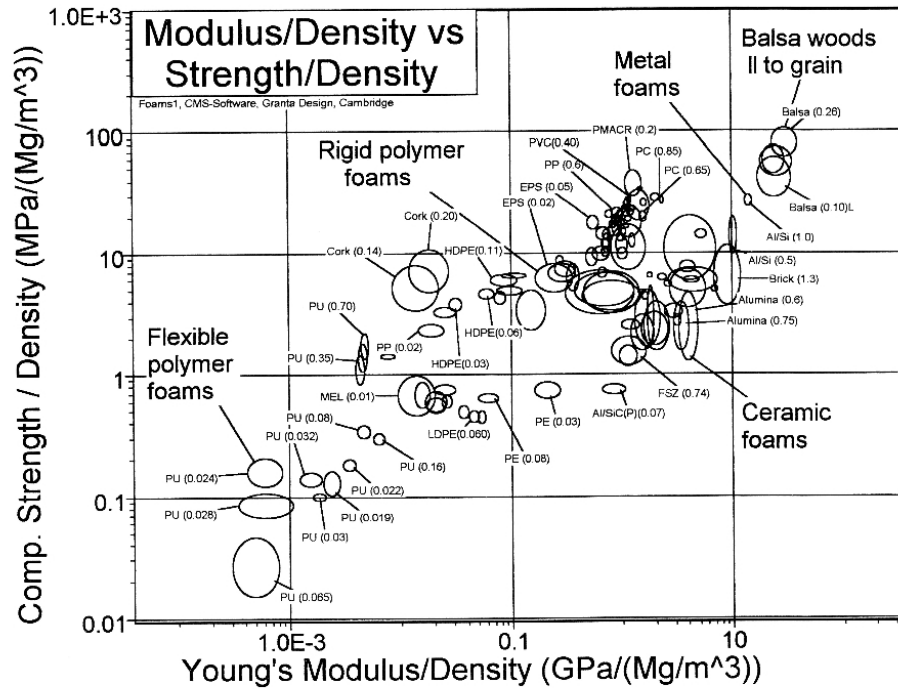
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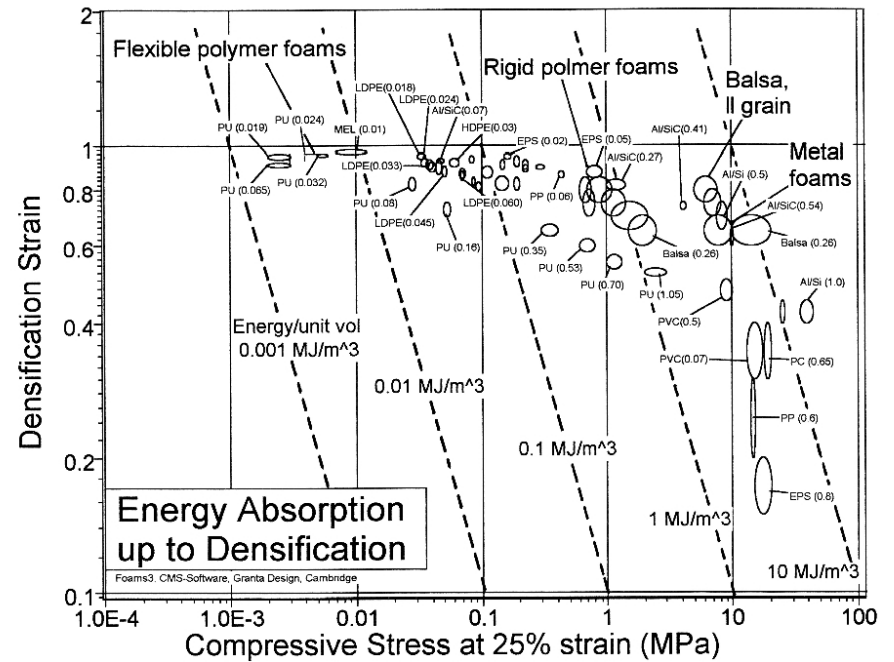
Ashby plot of Young's Modulus - Density © Granta Design. All rights reserved. This content is excluded from our Creative Commons license. For more information, see <http://ocw.mit.edu/help/faq-fair-use/>.



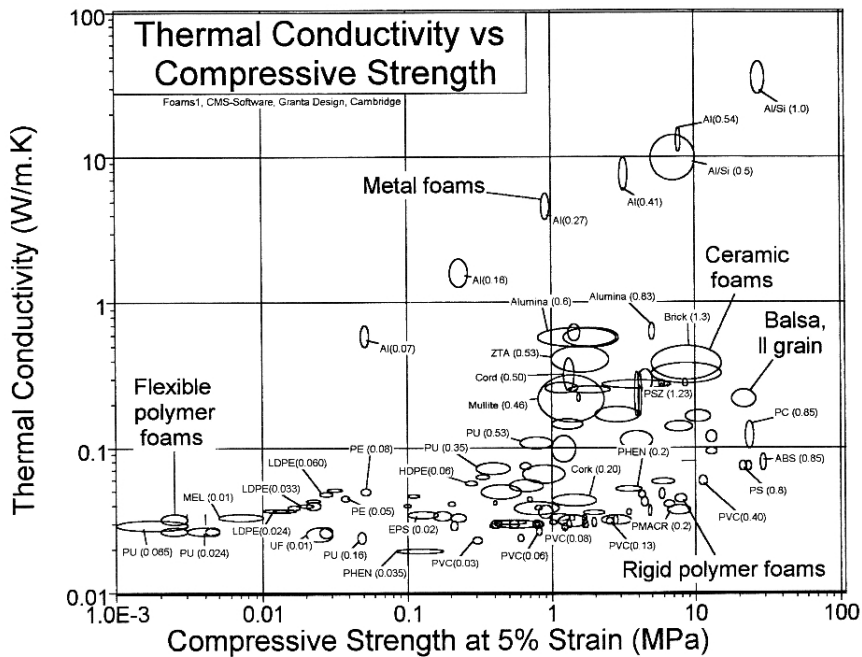
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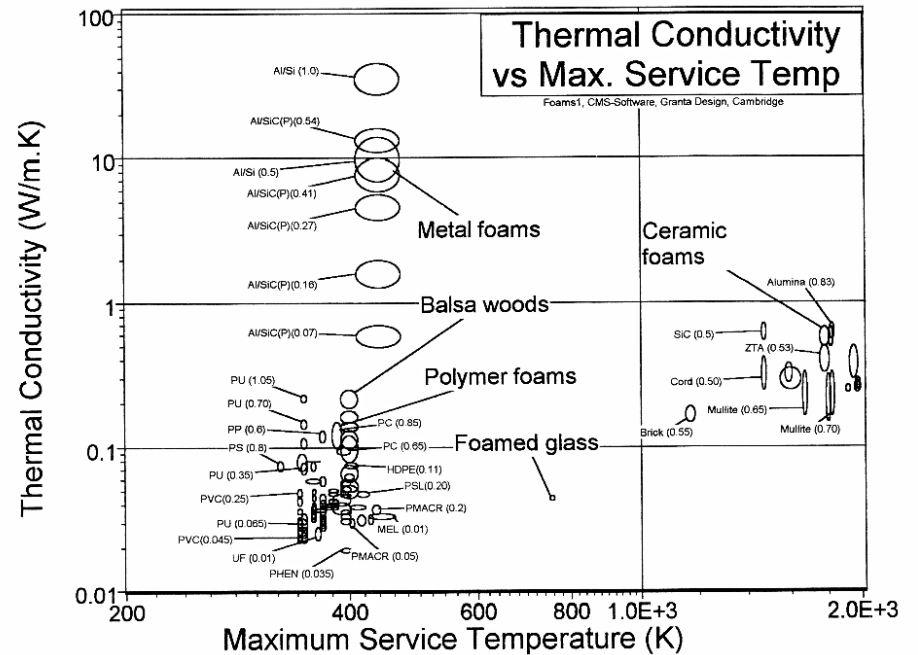
End grain balsa; metal foams
Useful for sandwich panels



Contours show energy absorption
per unit volume

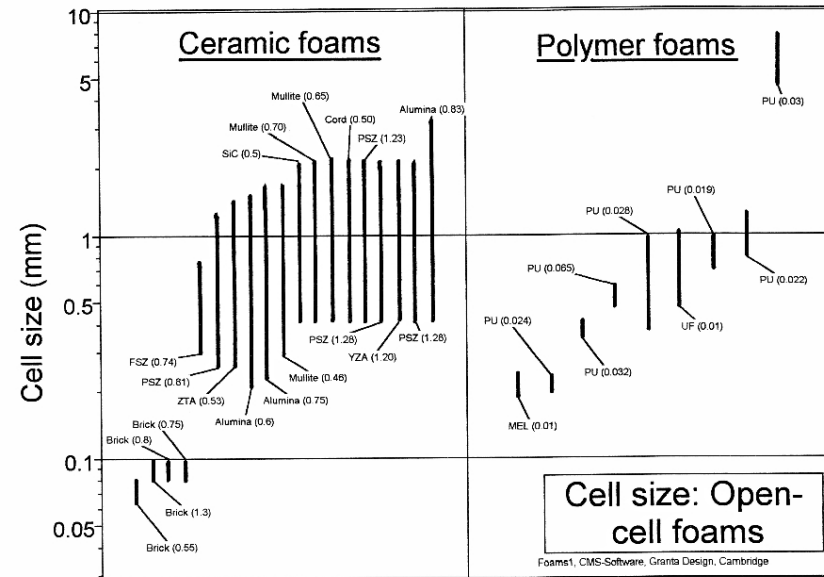
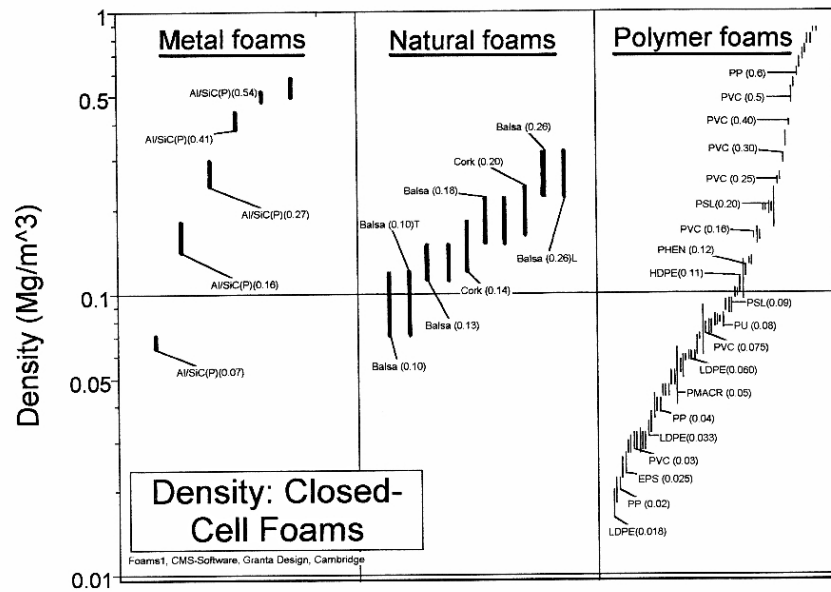


Thermal insulation applications;
Usually a constraint on strength, too



May also have a constraint on
maximum service temperature

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Buoyancy

Filtration and catalysis

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3.054 / 3.36 Cellular Solids: Structure, Properties and Applications
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