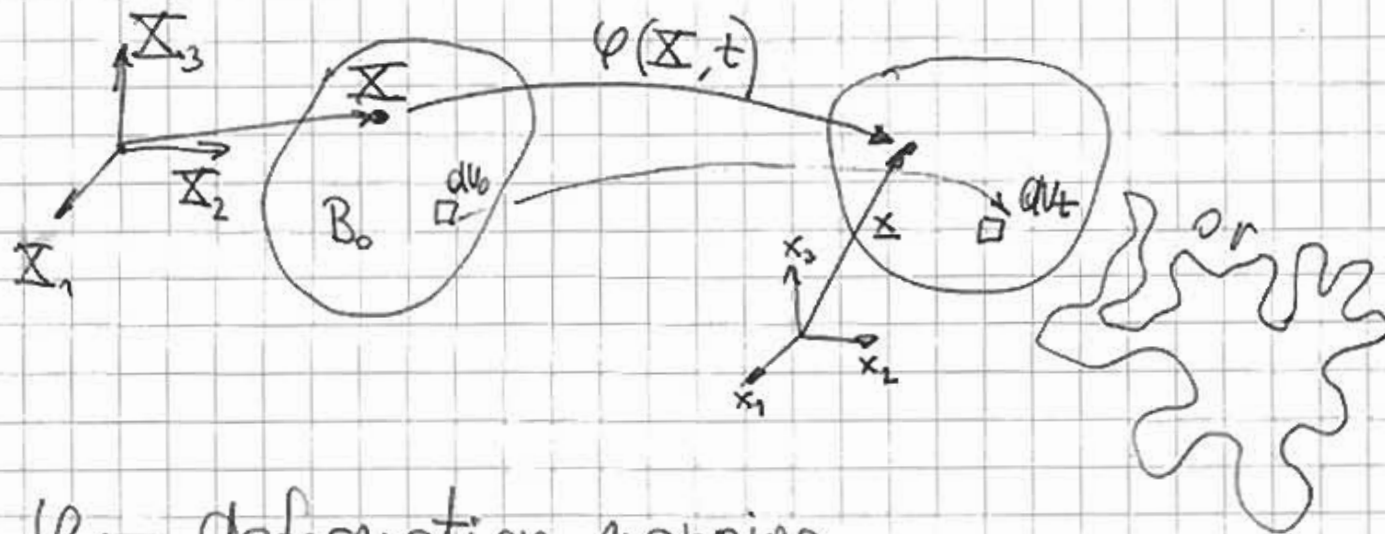
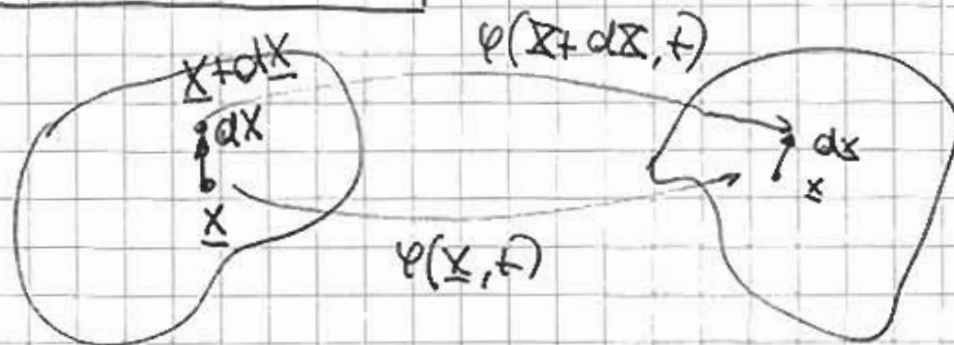


# FINITE ELASTICITY



$\varphi \equiv$  deformation mapping

$$\boxed{x_i = \varphi_i(\mathbf{X}, t)}$$



$$d\mathbf{x} = \varphi(\mathbf{X} + d\mathbf{X}, t) - \varphi(\mathbf{X}, t) \sim$$

$$\left[ \frac{\partial \phi_i(\mathbf{x}, t)}{\partial X_j^*} dX_j + \text{hot} \right]$$

$F_{iJ}(\mathbf{x}, t) \equiv \text{def. gradient}$

Metric changes

$$\begin{aligned} ds^2 = dx_i dx_i &= (F_{iI} dX_I) (F_{iJ} dX_J) \\ &= \underbrace{F_{iI} F_{iJ}}_{C_{IJ}} dX_I dX_J \end{aligned}$$

$C_{IJ} \equiv \text{Cauchy-Green def. tensor}$

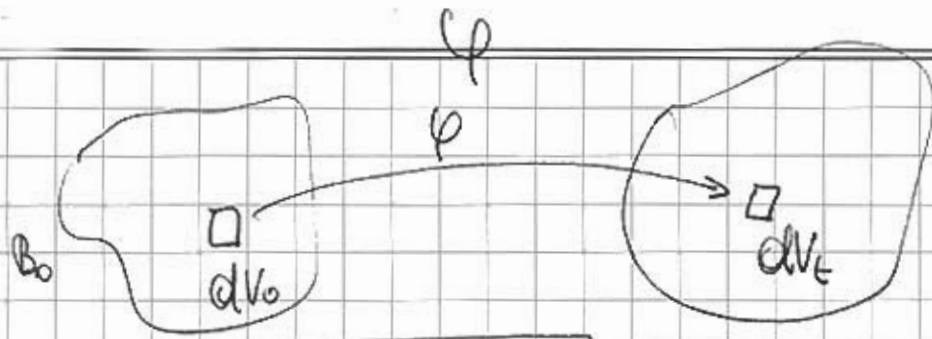
$$\boxed{C = F^T F}$$

$$ds^2 = dX_I dX_I$$

$$\frac{1}{2} (ds^2 - ds^2) = \frac{dX^T}{\cancel{14}} (C - I) dX \frac{1}{2}$$

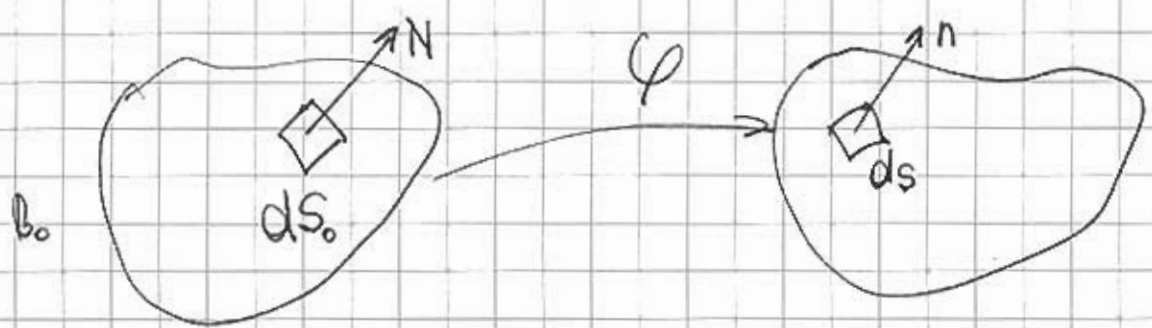
$$d\epsilon = dX^T E dX$$

$$E_{IJ} = \frac{1}{2} (C_{IJ} - I_{IJ})$$



$$\frac{dV}{dV_0} = \det(F) = J$$

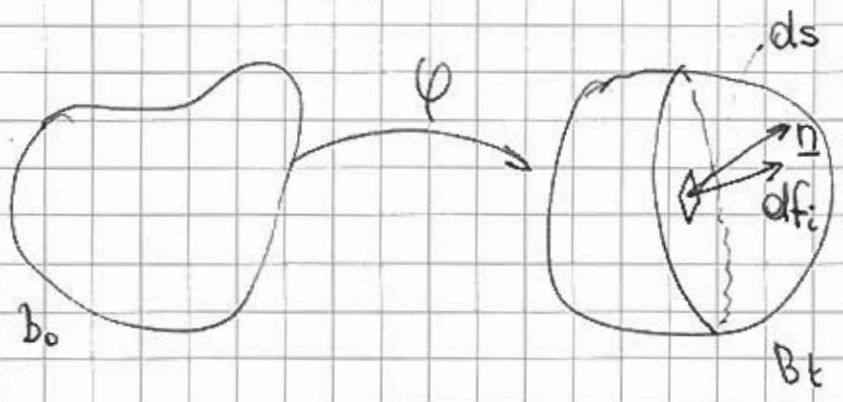
Jacobian of def.



Piola transformation

$$n_i ds = J N_I F_{Ii}^{-1} dS_0$$

### State of stress



$df_i \equiv$  absolutely continuous wrt area

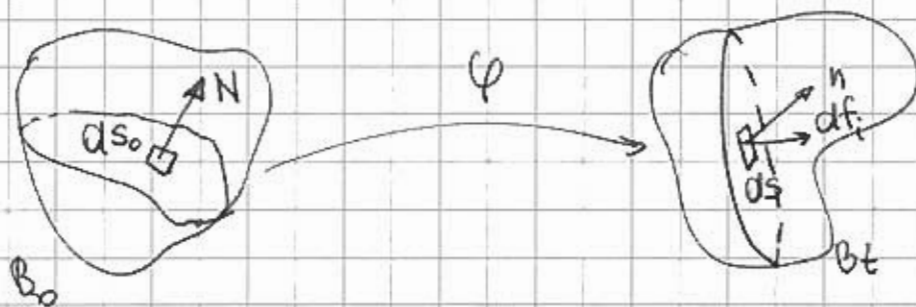
$$df_i = t_i ds$$

$t_i$ : <sup>spatial</sup> traction forces / unit deformed area

From Cauchy tetrahedron theorem:

$$t_i = \sigma_{ij} n_j$$

↑ Cauchy stress tensor



Define material tractions  $T_i = \frac{df_i}{dS_0}$

$$df_i = T_i dS_0 = t_i ds = \sigma_{ij} n_j ds$$

$$= \sigma_{ij} J N_I F_{Ij}^{-1} dS_0 \implies$$

$$T_i = P_{iI} N_I$$

$$P_{iI} = J F_{Ij}^{-1} \sigma_{ij}$$

1st Piola Kirchoff stress tensor

$$P = J \sigma F^{-T}$$

Def:  $df_I = F_{Ij}^{-1} df_j = S_{IJ} N_J ds_0$

2nd PK ~~stress~~  
stress tensor

$$S_{IJ} = J F_{Ii}^{-1} F_{Jj}^{-1} \sigma_{ij}$$

$$S = J F^{-1} \sigma F^{-T}$$

Kirchhoff stress

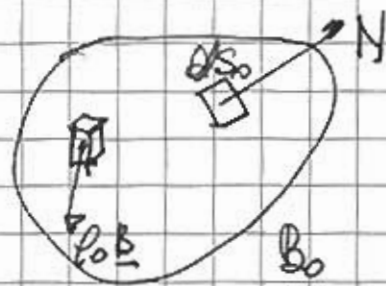
$$T_{ij} = J \sigma_{ij}$$

## Field equations

Linear momentum balance:

$$L_i = \int_{B_0} \rho_0 V_i dV_0$$

$$R_i = \int_{B_0} \rho_0 B_i dV_0 + \int_{S_0} \overbrace{P_{iI}}^{T_i} N_I dS_0$$



$$\frac{dL_i}{dt} = R_i \Rightarrow$$

$$P_{iJ,J} + \rho_0 B_i = \rho_0 A_i$$

$$\nabla_0 \cdot P + \rho_0 B = \rho_0 A$$

material gradient

$$V_i = \frac{\partial \varphi_i(X,t)}{\partial t} = v_i(X,t)$$

$$A_i = \frac{\partial v_i(X,t)}{\partial t}$$

defined over the  
reference config.  
happening on the spatial  
velocity (i)

Angular Momentum balance

$$\begin{array}{|l} \sigma = \sigma^T \\ s = s^T \\ \tau^T = \tau \end{array} \Rightarrow$$

Energy balance

$$\dot{u} = S_{IJ} \frac{1}{2} \dot{C}_{IJ} = P_{iJ} \dot{F}_{iJ} = T_{ij} \dot{d}_{ij}$$

deformation power / unit UNDEFORMED volume



$$d_{ij} = \text{rate of det. tensor} = \frac{1}{2} (l_{ij} + l_{ji})$$

$$l_{ij} = v_{i,j} \equiv \text{spatial velocity gradient}$$

$$l = \dot{F} F^{-1}$$

## Nonlinear elastic solid

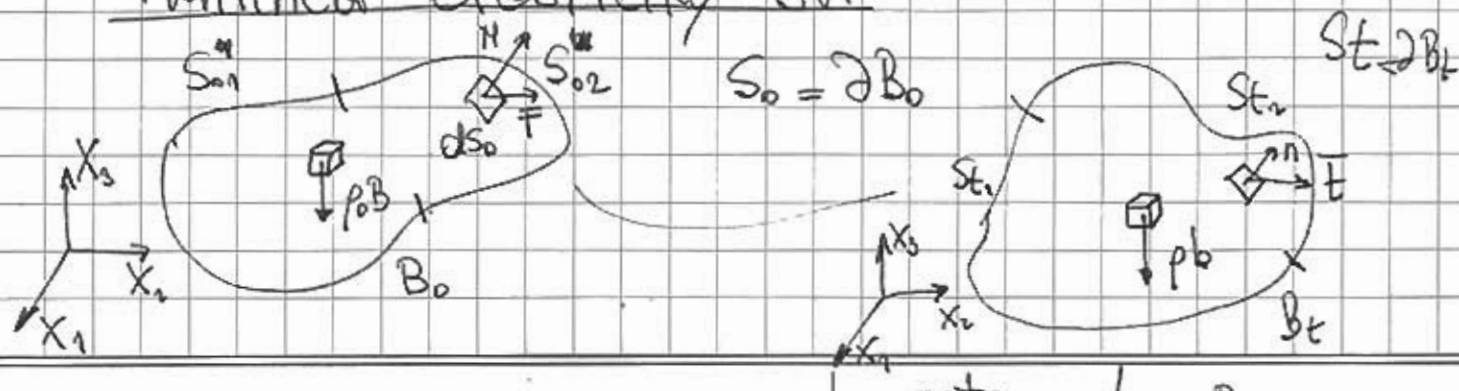
$P_{iJ} \dot{F}_{iJ}$  perfect differential

$\Leftrightarrow \exists W(F) \equiv$  strain energy density (per unit undeformed volume)

$$P_{iJ} = \frac{\partial W}{\partial F_{iJ}}$$

Most general constitutive relations for nonlinear elastic solids.

## Nonlinear elasticity BVP



note:  $b = B$  since  $\rho dt b = \rho_0 dt b B_0$

Field eqs (Lagrangian setting)

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1) Compatibility:

$$\left. \begin{aligned} F_{iJ} &= \ell_{i,J} && \text{in } B_0 \\ \ell_i &= \bar{\ell}_i && \text{on } S_{01} \end{aligned} \right\}$$

2) Equilibrium:

$$\left. \begin{aligned} P_{iJ,J} + \rho_0 B_i &= \rho_0 A_i && \text{in } B_0 \\ P_{iJ} N_J &= \bar{T}_i && \text{on } S_{02} \end{aligned} \right\}$$

3) Constitutive:

$$P_{iJ} = \frac{\partial W(F)}{\partial F_{iJ}} \quad \text{in } B_0$$